

## Super Wide Band Cavity With An All-Pass Network

H.Tamura, S.Ninomiya, \*K.Noda and K.Sato

*Research Center for Nuclear Physics (RCNP), Ibaraki, Osaka 567-0047, Japan*  
*\*National Institute of Radiological Sciences (NIRS), Chiba 263-8555, Japan*

A tuning-free cavity with a bridged-T type all-pass network has been developed for an ion synchrotron [1][2] as shown in Fig.1. As for the characteristic of this cavity with an all-pass network, output impedance is equal to input one. The sufficient condition values of parameter are as follows

$$Z_2 = \frac{R^2}{2Z_1}, \quad Z_3 = 4Z_1 \quad (1)$$

LC expression as follows

$$L_2 = \frac{C_1 R^2}{2}, \quad C_2 = \frac{2L_1}{R^2}, \quad L_3 = 4L_1, \quad C_3 = \frac{C_1}{4} \quad (2)$$

The acceleration voltage of this cavity has the characteristic curve which looks like a band pass filter. Since the circuits of bridged-T type all-pass network are divided low and high pass filter, the values of  $f_{\min}$  and  $f_{\max}$  are roughly estimated to  $f_{\min} \cong R/(4\pi L_1)$ ,  $f_{\max} \cong 1/(\pi R C_1)$ .

The accurate values are as follows

$$f_{\min} = \frac{1}{2\pi\sqrt{L_1 C_1}} \left\{ \sqrt{1 + \frac{L_1}{R^2 C_1}} - \frac{1}{R} \sqrt{\frac{L_1}{C_1}} \right\} \quad (3)$$

$$f_{\max} = \frac{1}{2\pi\sqrt{L_1 C_1}} \left\{ \sqrt{1 + \frac{L_1}{R^2 C_1}} + \frac{1}{R} \sqrt{\frac{L_1}{C_1}} \right\} \quad (4)$$

$$f_0 = \frac{1}{2\pi\sqrt{L_1 C_1}} \quad (5)$$

Comparing the acceleration gap voltage phase to input phase, a phase difference change continuously between  $f_{\min}$  and  $f_{\max}$  from +90 for the -90 degrees as shown in Fig.2.

We selected parameters with values of  $L_1 = 16.83\mu H$ ,  $C_1 = 240pF$  so that an acceleration gap voltage could generate between 0.1 and 60MHz. Then, this cavity voltage was generated between 0.1 and 32MHz as shown in Fig.3.

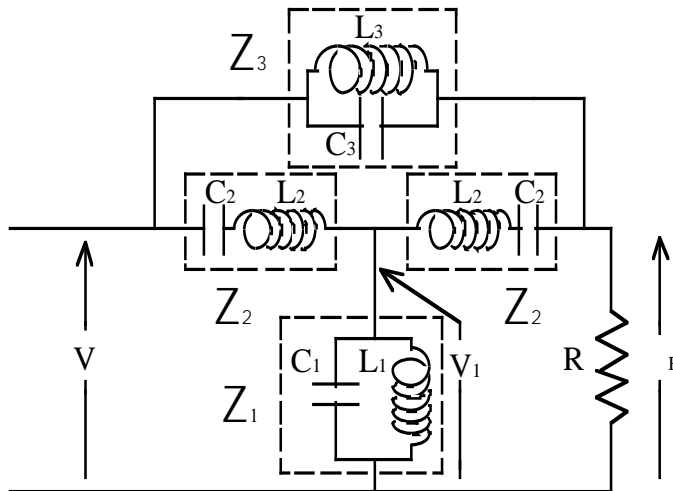


Fig.1; A bridged-T type all-pass network ( $Z_1$  is basic cavity.)

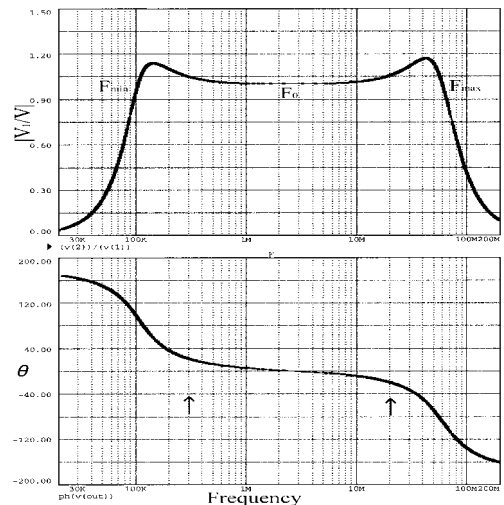


Fig.2; Low-level RF test results  $|V_1/V|$  and phase

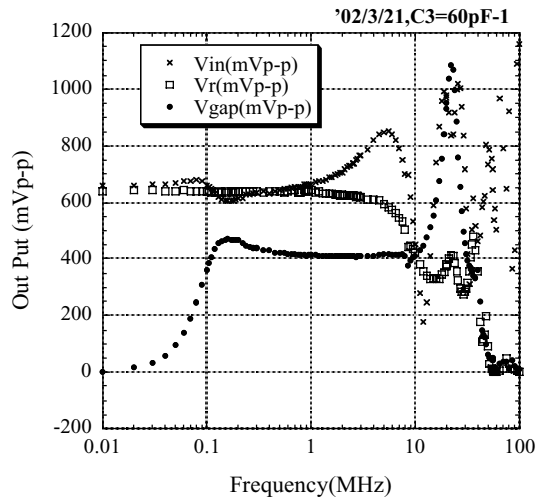


Fig.3; Low-level RF test results of the cavity (Source V/ Terminal Resister  $V_R$ / Cavity voltage)

The  $f_{\min}$  value from equation (3) is almost the same as measured 0.1MHz. But, the  $f_{\max}$  value from (4) is different from measured 32MHz. The parameter  $L_2$  values that it wasn't measured may be wrong. And  $L_2$  value is very little one. As for the measurement of  $L_1$ ,  $C_1$  of the circuit parameters, accurate value  $L_1 = 15.9\mu H$  can be calculated from the measurement value by using a Vector Impedance Meter, and  $C_1$  value was adjusted  $C_1 = 240pF$ . But, the measurement of the  $L_2$  of the component seems to be very difficult. Then, it influence of the value of  $f_{\max}$  if the value of  $L_2$  is different from the design value ( $L_2 = 57.9nH$ ). The measured  $L_2$  value is less than 362nH.  $F_{\max} = 29.3MHz$  is calculated by  $L_2 = 362nH$ . A frequency band width of accelerator gap voltage is smaller than design value.

This cavity can generate sawtooth-wave rf-field. A sawtooth-wave is suitable for production of short bunched beam compared with a sine wave. A short-bunched beam with 370 ns at FWHM (full width at half maximum) was gotten in using the sawtooth-wave (500V<sub>p-p</sub>), while that with 480 ns in the sine wave (500V<sub>p-p</sub>). As shown in Fig.4, 5 (Horizontal scale is 400 ns/div at  $f = 1.042180MHz$ .)

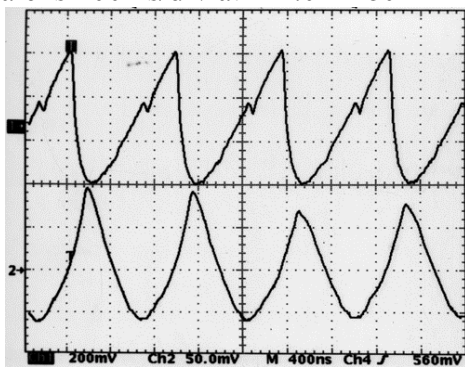


Fig.4; Sawtooth-wave and bunched beam

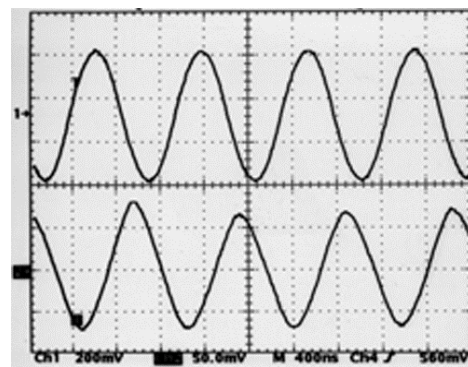


Fig.5; Sine wave and bunched beam

## Reference

- [1] H.Tamura et al., RCNP Annual Report 2000 p.104
- [2] H.Tamura et al., Procs. of the 12<sup>th</sup> Symposium on Accelerator Science and Technology,